



Experimental Investigation of Solar Room Heater for Commercial Purpose

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Abstract:

According to the present era the requirement of the energy is continuously increasing. At the earth surface abundant quantity of heat is available but not in useful form, one of the main source of this energy is Solar which is available free of cost. On the basis of this theory we have designed a solar room heater by using tin cans soldered with spiral wire for increasing heat transfer between air and solar heat present in the collector. After designing the experimental set up experiment will be carried out for finding the outlet temperature, velocity of air for calculating heat transfer and pressure drop, heat transfer characteristics across the solar air heater. In this study, we have concluded the temperature of inlet air will improve around 17°C to 20°C without using any external device like blower and fans.

Keywords: Solar Room Heater, Tin Cans, Thermocots, Heated Air, Thermometer.

1 Introduction

In these day world is started move towards the renewable energy resources due high depletion of the fossil fuels and increasing rate of petrol, diesel and lot of environment and health problem faced by human being. The total energy from the fossil fuels is only 1% of the energy coming on the earth by sun in one day. **Sukhatme S.P. in 2003** concluded that wider spacing tube had higher efficiency than lesser spacing tube. **M.K. Mittal et.al.2005** the roughened solar room heater performed better than conventional smoother solar room heater. He also concluded that increase in efficiency due to use of inclined roughened rib in pipe of solar heater. **Varun et. al. (2007)** determined the heat transfer, friction factor by taking the inclined and transverse ribs over the absorber plate in between the range of reynolds number of 2000 to 14000 at defined relative roughness pitch, relative roughness height. **R.P. Saini and Jitendra Verma (2008)** improved the heat transfer rate by providing roughness underside to the absorber plate duct in the range of reynolds number from 2000 to 12000 with relative pitch 8 to 12 and relative height 0.018 to 0.037. **S.V. Karmare and A.N. Tikekar (2008)** have been investigated the effect of producing artificial roughness on pumping power and thermodynamic performance parameter in the range of Reynolds number from 3600 to 17000 at different-2 relative pitch, relative height. **Santosh B. Bopche and Madhukar S. Tandale (2009)** have been determined the heat transfer coefficient, friction factor in the U shaped roughened surface by making roughened wall heated and other three walls insulated. The experiments conducted on the range of Reynolds number 3800 to 18000 at different-2 hydraulic diameter. **R.S. Gill et. al. in 2012** concluded that ambient temperature, stagnation temperature, solar radiation variation

through out the day in single glazed, double glazed and packed bed air heater. He also concluded that single glazed room heater give better performance in summer and double glazed room heater performed well in winter. **Vijay et.al.(2018)** experimental investigations was related to the artificial roughened solar heater. In this experiment he observed the effect of different variable of roughness (height, width, angle, pitch etc) on the heat transfer coefficient and friction factor for calculating the efficiency of collector, exergetic efficiency of air flow out of collector. **M. Ansari et.al.(2018)** in his experiments set developed the rib type solar model in which optimized height of the rib is find out and concluded that taller height rib will produce the high turbulence at low mass flow rate. **Deep Singh Thakur et. al.(2016)** done the 2D CFD analysis over artificial roughened solar air heater with novel hyperbolic ribs. The performance of novel hyperbolic ribs are also validated with rectangular, triangular and semicircular ribs performance at different-2 reynolds number and checked upto the 10000. **M. Cuzminschi et. al.(2017)** done the experimental and CFD analysis on solar air heater for residential purpose. It is fully depends on the natural convection phenomena and can be used for drying the seed, nuts, fruits. **Simarpeet Singh (2017)** done the numerical simulation on ANSYS FLUENT(16.2) and getting the pressure field, velocity field, temperature field to determine the pumping power, nusselt number and heat transfer at solar constant of 500W/m² in range of Reynolds number from 3800 to 14000. He also see the variation of nusselt number with Reynolds number and found that 10000 reynold number the nusselt number is significantly improved. **Ali Heydariaet. al.(2018)** design a model of solar air heater in which air is flowing at helical path through a triangular section. After designing the apparatus experimental and numerical experimentation investigation is done and same results is compared for finding the better design. **A.E. Kabeel et.al.(2018)** compared

the performance of conventional air heater, baffled glazed-bladed entrance air heater (BGBSAH) at the same operating conditions. In addition he found that baffled glazed blade efficiency is increased from 29.91 to 51.69% with 800 baffled compared to conventional solar air heater. **Inderjeet Singh et.al.(2018)** used the roughened surface for breaking the laminar sub layer at the absorbing surface in turbulent layer for improving heat transfer characteristics and improve overall efficiency.

2.Experimental Set UP.



Figure-1: Experimental Set up of Solar Air Heater

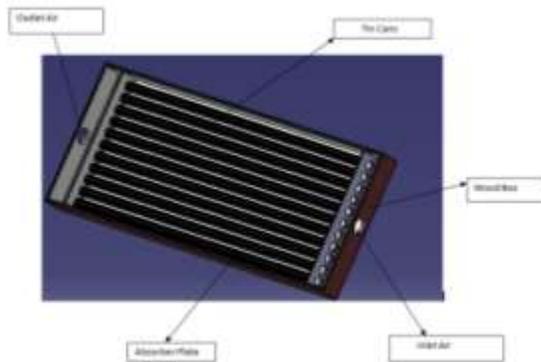


Figure-2: Model of Experimental Set Up

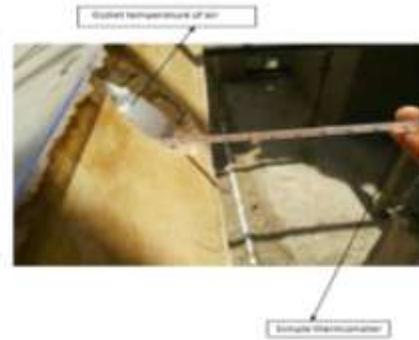


Figure-3: Measurement of Temperature at outlet of solar air heater

3. The experimental set up contain following parts

Tin can (10 cm diameter): used for movement of air from inlet to outlet. The air is moved due to pressure difference occur due to inclination of solar air heater at window of the room.

Wood board: is used to support whole frame the dimensions of 225cm*95cm. The front end of board contains the hole for entrance for the inlet air.

Thermocouple: It is located at both side of the board have the 11 hole support the tin can painted with black color.

Transparent Glass Plate: A glass sheet 5mm thickness is provided to trap high wavelength of radiation coming from the top glass plate. It works like as the green house chamber.

Absorber Plate: it is the 1mm thick copper sheet black painted so that its absorvity is around 100%.

Insulation: Mineral wool of 8cm is used for the perfect insulation from bottom site for stopping heat transfer by convection, conduction.

4. Mathematical Equation

Heat energy from Sun passes through the cover plate reached on the absorber plate. The absorber plate are black painted so most of the energy is absorbed by it rest of the energy is reflected back to atmosphere some part of it is transmitted to the bottom plate. Therefore for writing the model equation we have write the energy balance among absorber plate, cover plate, bottom plate , atmosphere present around the solar air heater. These equation taken from book of solar energy written by **S.P. Sukhatame[4]**.

Solar energy absorbed by Absorber Plate= Heat transfer to fluid air by convection + Heat transfer to fluid air by convection+ heat transfer to bottom plate by radiation

$$SL_2 dx = u_t L_2 dx (T_{pm} - T_{bm}) + \square_{fp} L_2 dx (T_{pm} - T_f) + \sigma L_2 dx (T_{pm}^4 - T_{bm}^4) / (\frac{1}{\epsilon_p} - \frac{1}{\epsilon_b} - 1) \tag{1}$$

For bottom plate

$$\frac{\sigma L_2 dx (T_{pm}^4 - T_{bm}^4)}{\frac{1}{\epsilon_p} - \frac{1}{\epsilon_b} - 1} = \square_{fb} L_2 dx (T_{bm} - T_f) + u_b L_2 dx (T_{bm} - T_a) \tag{2}$$

For Air stream

$$m \cdot c_p dT_f = \square_{fp} L_2 dx (T_{pm} - T_f) + \square_{fb} L_2 dx (T_{bm} - T_f) \tag{3}$$

Radiation Heat transfer Coefficient

$$h_r = 4\sigma T_{av}^3 / (\frac{1}{\epsilon_p} + \frac{1}{\epsilon_b} - 1) \tag{4}$$

$$T_{av} = \frac{T_{pm} + T_{bm}}{2} \tag{5}$$

Useful heat gain

$$q_u = F_R A_p [S - U_i^{II} (T_{fi} - T_a)] \tag{6}$$

Heat Transfer

$$F_R = m C_p / U_i^{II} A_p \left[1 - e^{-\left\{ \frac{F^I U_i^{II} A_p}{m C_p} \right\}} \right] \tag{7}$$

Kays Equation

$$N_{u_i} = 0.0158 R_g^{0.8} \tag{8}$$

Malik and Buelow Equation

$$N_{u_i} = 0. \frac{0.1344 R_g^{0.75}}{1 - 10586 R_g^{-0.125}} \tag{9}$$

Equivalent Diameter

$$d_e = \frac{4A}{p} \tag{10}$$

Blausius Equation

$$f = 0.079 R_g^{-0.25} \tag{11}$$

5. Experimental Reading

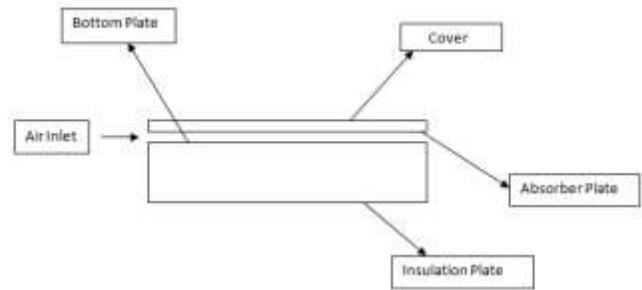


Figure-4: Arrangement of Absorber plate, Cover plate, Bottom Plate

Table-1: Experimental reading

S.No.	Inlet Temp (°C)	Outlet Temp (°C)	ΔT (°C)	velocity	Mass flow rate of air Kg/sec
1	40	57 °C	17 °C	0.4246	0.040
2	35	50 °C	15 °C	0.478	0.045
3	33	46 °C	13 °C	0.5626	0.053
4	30	40 °C	10 °C	0.6263	0.059

Table-2: On the basis of experimental reading calculation of heat transfer, pressure Drop

Reynold Number ($\rho V d_e / \mu$)	Friction Factor $f = 0.079 R_g^{-0.25}$	Pressure Drop $\delta P = 2f \rho L V^2 / d_e$	Nusselt Number $N_{u_i} = 0.0158 R_g^{0.8}$
2567	0.011098	0.108	8.437
2887	0.01078	0.133	9.2686
3401	0.010344	0.1767	10.56
4544	0.009622	0.2	13.323

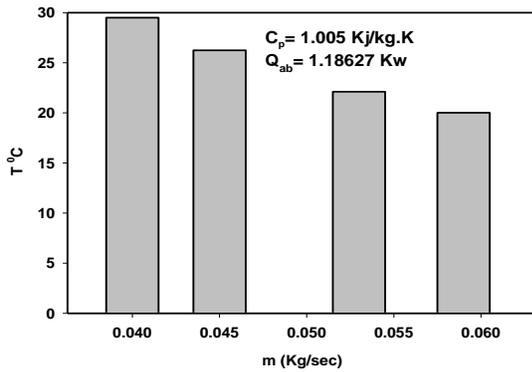


Figure-5: Variation of Outlet Temperature with Mass flow rate.

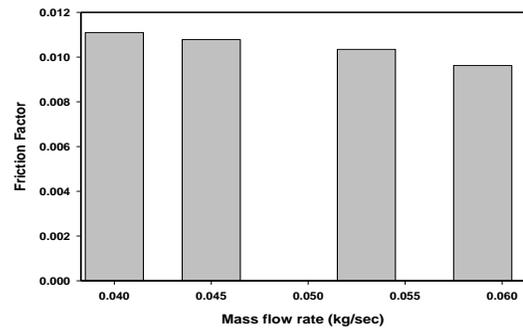


Figure-7: Variation of Friction Factor with Mass flow

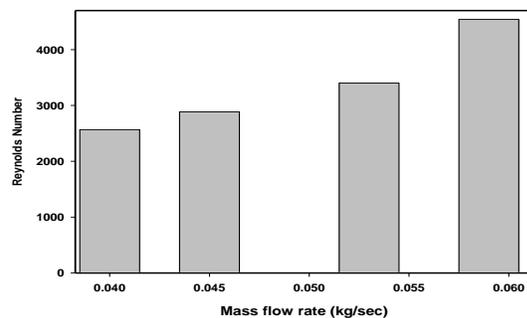


Figure-6: Variation of Reynolds Numaber with Mass flow rate.

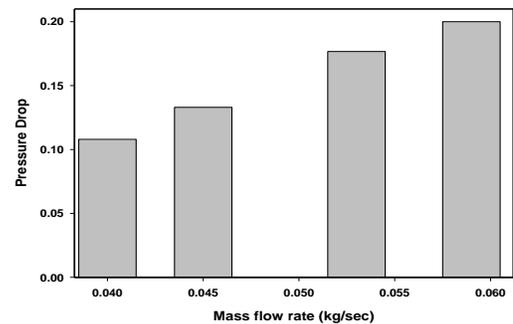


Figure-8: Variation of Pressure Drop with Mass flow rate.

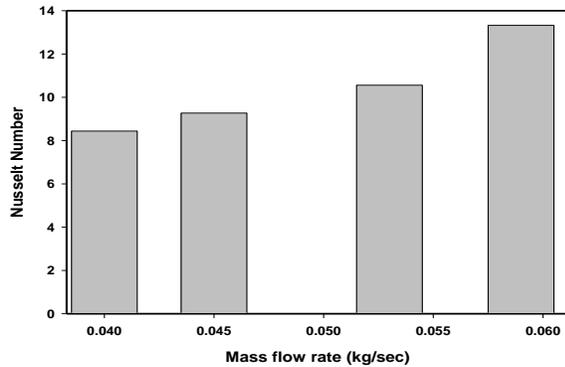


Figure-9: Variation of Nusselt Number with Mass flow rate.

6. Conclusion

In this paper we have concluded the following observation at the time of experimentation.

- 1- Figure-5 concluded that the temperature at outlet reduced due to incensement of mass flow rate because most of the heat absorbed by solar plate is transmitted to the air flow through the spiral tin can pipe.
- 2- Figure-6 shows the variation of Reynolds number significantly by small increment of mass flow rate.
- 3- Figure-7 shows that when mass flow rate increase friction factor little bit improve but in figure-8 pressure drop increased significantly due to increment in velocity.
- 4- Figure-9 shows the increment of nusselt number with mass flow rate. So we can concluded that due to increase in nusselt number heat transfer coefficient also improved result in several times heat transfer.

The only demerit of solar energy in winter season is reduced because sun rays are slanting in the northern hemisphere so intensity of heating on earth is less. The running cost of solar heating is very less only maintenance cost is there.

References

- [1] The Solar Thermal Air Heating and Cooling Association (STA), <http://solarairheating.org.au/>
- [2] R.S. Gill, Sukhmeet Singh, Parm Pal Singh, Lowcostsolarairheater, Energy Conversion and Management,2012
- [3] M.K. Mittala, Varuna, R.P. Saini, S.K. Singal, Effectiveefficiency of solar airheatershavingdifferenttypes of roughnesselementsontheabsorberplate, Elsevier, Energy 32 (2007) 739–745, September 2005
- [4] Sukhatme S.P., "Solar Energy: Principles of ThermalCollectionsandStorage", TataMcGraw-Hill, NewDelhi2003.
- [5] The Solar Thermal Air Heating and Cooling Association (STA), <http://solarairheating.org.au/>
- [6] R.S. Gill, Sukhmeet Singh, Parm Pal Singh,Low cost solar air heater,Energy Conversion and Management,2012
- [7] M.K. Mittala, Varuna, R.P. Saini, S.K. Singal, Effective efficiency of solar air heaters having different types of roughness elements on the absorber plate, Elsevier, Energy 32 (2007) 739–745,September 2005
- [8] Karmare SV, Tikekar AN. Experimental investigation of optimum thermo hydraulic performance of solar air heaters with metal rib grits roughness. Sol Energy 2009;83:6–13.
- [9] Saini RP, Verma J. Heat transfer and friction factor correlations for a duct having dimple-shape artificial roughness for solar air heaters. Energy 2008;33:1277–87.
- [10] Varun, Saini RP, Singal SK. Investigation of thermal performance of solar air heater having roughness elements as a combination of inclined and transverse ribs on the absorber plate. Renew Energy 2008;33:1398–405.
- [11] ManashDeyEffect of Artificial Roughness on Solar Air Heater: An Experimental Investigation, Int. Journal of Engineering Research and Application Vol. 3, Issue 5, Sep-Oct 2013, pp.88-95.
- [12] Bopche SB, Tandale MS. Experimental investigations on heat transfer and frictionalcharacteristics of a turbulator roughened solar air heater duct. Int J Heat MassTransf 2009;52:2834–48.
- [13] Thakur DS, Khan MK, Pathak M. Performance evaluation of solar air heater with novel hyperbolic rib geometry. Renew Energy 2017;105:786–97. <http://dx.doi.org/10.1016/j.renene.2016.12.092>.
- [14] Singh S. Performance evaluation of a novel solar air heater with arched absorber plate. Renew Energy 2017;114:879–86. <http://dx.doi.org/10.1016/j.renene.2017.07.109>.
- [15] Kabeel AE, Khalil A, Shalaby SM, Zayed ME. Investigation of the thermal performances of flat, finned, and v corrugated plate solar air heaters. J Sol Energy Eng2016; 138:051004. <http://dx.doi.org/10.1115/1.4034027>.
- [16] Singh A, Singh S. CFD investigation on roughness pitch variation in non-uniform cross-section transverse rib roughness on Nusselt number and friction factor characteristics of solar air heater duct. Energy 2017;128:109–27.
- [17] Singh I, Singh S. CFD analysis of solar air heater duct having square wave profiled transverse ribs as roughness elements. Sol Energy 2018;162:442–53. <http://dx.doi.org/10.1016/j.solener.2018.01.019>.