

Design and Simulation of MEMS Moisture Sensor Using COMSOL Multiphysics Software

Muhamad Nazrin Ismail¹, Noriah Yusoff^{2*}, Nor Hayati Saad³, Amirul Abd Rashid⁴

^{1 2 3 4}Faculty of Mechanical Engineering, Universiti Teknologi MARA, 40450 Shah Alam

*Corresponding author E-mail: noriah Yusoff@salam.uitm.edu.my

Abstract

Micro-electro-mechanical system (MEMS) is a hybrid technology that combines electronic, electric and mechanical technology in a micron-size system. This allowed for higher performance and multifunction devices fabricated at much lighter weight and cost effective. One of the major application of MEMS is in sensor devices area. This paper highlight the simulation study of a typical moisture sensor fabricated from Tungsten Interdigitated (IDE) MEMS device. Using COMSOL Multiphysics software, the moisture sensor was modelled based on the current material and physical dimension and layout. The model then go through validation proses to its sensitivity performance against the experimental result. Subsequently, the optimization on sensor sensitivity was carried out by varying the model parameters including the sensor physical dimension, working temperature and humidity. The simulation result suggest that the sensor sensitivity is highly correlated to the electrode distance value. The average sensitivity of the sensor improved to ~48% better when the distance between reduced to 50% from 6 micron to 3 micron tested at temperature between 25 °C to 45 °C. This information is valuable as the input to the sensor designer in finalizing the MEMS physical layout in producing highly sensitive moisture sensor devices.

Keywords: COMSOL; MEMS; moisture sensor; capacitance; interdigitated device.

1. Introduction

The electronics industry have gone through huge advancement beyond the More's law prediction. One of the significant breakthrough was in MEMS technology where it convert any physical changes, events and parameters to mechanical, electrical and optical signals and vice versa. The advantage of integrating multiple function of system in smaller footprint has enabled the production of smaller, lightweight and low consumption devices. The application of MEMS can be found in every modern gadget of human lifestyles including computer, telecommunications, automotive and transportations, healthcare and others. The architecture and operating principle of MEMS is by utilizing micro scale features of electromechanical, electronics, optical and biological components however still required optimization in their design, analysis and fabrication [1].

The main components in MEMS consists of microsensor, microactuator, microelectronics and microstructure (refer to Fig.1). Microsensors is consider as the input for MEMS system where it is used to detect any changes in the system's environment by measure the thermal, mechanical, magnetic, chemical or electromagnetic, information of phenomena. The information measured by the sensor will be processed by microelectronic and send the signal to the microactuator to create form of changes to the environments [2].

1.1 Interdigitated (IDE) Sensor

Interdigitated sensor follows the rule of two parallel plate capacitor, where one side of both of the electrodes will be facing up for the material under test [4]. Fig. 2 shows the electric field line of

the parallel plate capacitor and an interdigital sensor. The electrical field lines generated by the sensor will penetrate into the material under test and the impedance of the sensor will be changed. Interdigital sensor behaves as capacitor in which the capacitive reactance becomes the function of the system properties and the system properties can be evaluated. AC voltage source will be applied between positive terminal and negative terminal as an excitation voltage. The electric field is created and it penetrates from positive terminal to negative terminal as can be seen in Fig. 2.

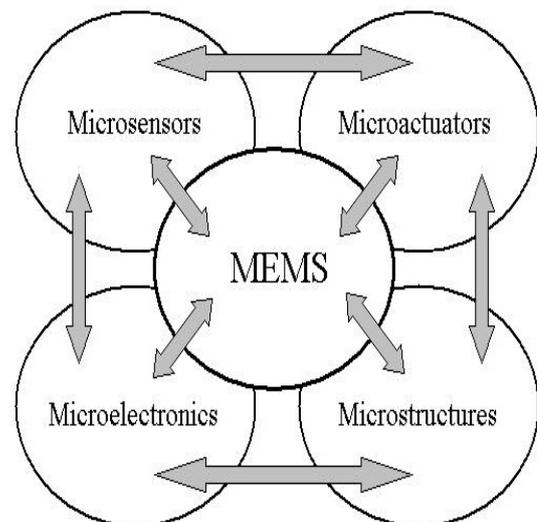


Fig. 1: A schematic illustration of MEMS components and their interdependence [3]

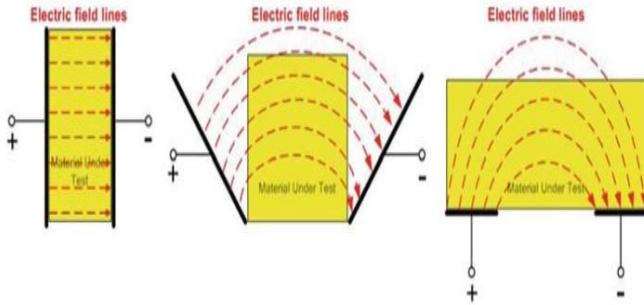


Fig. 2: Electric field lines of parallel plate capacitor and on coplanar interdigital sensors [4]

The configuration of the interdigital electrodes can be repeated many times in order to get a stronger signal. Since the repeated configuration parallel in-plane electrodes look like a digit-like or finger-like thus, the term “interdigital” is used. Fig. 3 shows a typical conventional interdigital electrodes sensor platform.



Fig. 3: Configuration of conventional planar interdigital sensor [4]

The distance between the two consecutive electrodes of the same polarity influenced the depth penetration of the electric field or also known as the fringing fields. Fig. 4 shows the side view of interdigital sensor and the penetration of the electric field. Also Fig. 4 exhibits the pitch length (l_1, l_2, l_3) with different depth of penetration. Research by [4] reported that when the electric field depth penetration of the electric field is increased, the strength of the electric field is weakened. Theoretically, the fringing electric field is weakening as the distance between the electrodes is increasing.

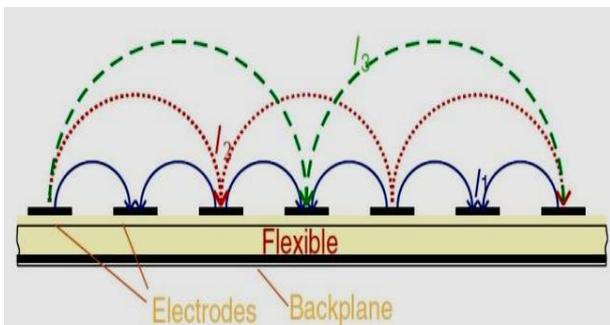


Fig. 4: Electric field formed between positive and negative electrodes for different pitch length (l_1, l_2, l_3) [4]

2. Method

In this research, the framework of the overall activities conducted in this study is described in Fig.5. The simulation model is validated by comparing the simulation results against the experimental data obtained from the previous study in [5].

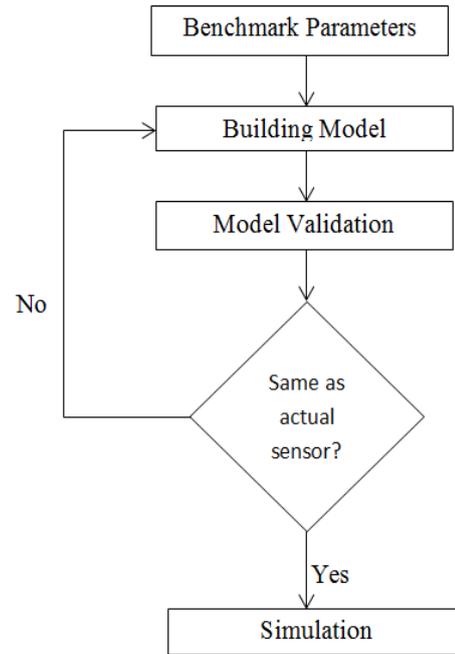


Fig. 5 Methodology Flow Chart

2.1. Benchmark Parameter

The benchmark parameter setting is according to the actual parameters of the moisture sensor of the research in [5]. This benchmark parameters is used as the model building setting of the moisture sensor using COMSOL Multiphysics software. The parameters include the size, the material used and also other model building input that are required for the moisture sensor modelling process.

2.2. Building Model

The simulation model is constructed according to the benchmark parameters; refer to Fig. 8. The model was built by using COMSOL Multiphysics software according to the dimension and the boundary conditions that were set for the moisture sensor accordingly.

2.3. Validation

The simulation results; the capacitance reading is compared against the experimental results obtained in research [5] hence the validated the MEMS moisture sensor that was built in COMSOL Multiphysics software. The validation process is prerequisite in simulation studies because the constructed model must be representing the actual condition of the subject matter in order to get a reliable simulation output result. Then, the validated model is used a reference model. Thus, any changes made on the investigated parameters were compared and analyzed accordingly.

2.4. Improvisation

In improvisation process, the parameters of the validated model (reference model) were changed in terms of the size of the electrodes and the distance between the electrodes in order to optimize the performance of the sensor which is the sensitivity of the capacitance value. The simulation results of the improvised model were compared against the reference model and the performance of both conditions were analyzed.

MEMS Moisture Sensor Modelling

Fig. 6 shows the MEMS moisture sensor that was built in COMSOL Multiphysics software. The MEMS moisture sensor has 126 fingers pair with equidistance of each pair. The electrodes are made of Tungsten and its material properties is set according to Table 1. The first layer under the electrodes is the silicon dioxide and the bottom layer is silicon substrate. In this study, the model is built according to a pair of the electrodes that consists of a terminal electrode and a ground electrode respectively.

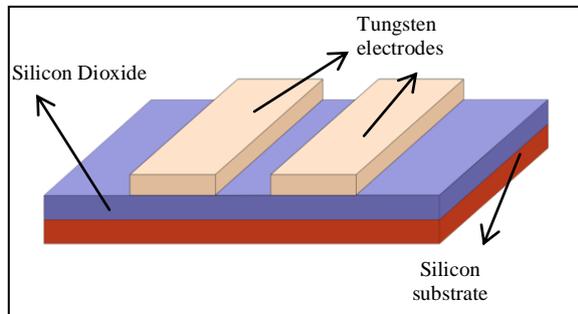


Fig. 6: Schematic Diagram of the MEMS Moisture Sensor

Table 1: Material properties of Tungsten

Property	Value	Unit
Relative Permittivity	30	1
Electrical Conductivity	2.00E+07	S/m
Coefficient of Thermal Expansion	4.50E-06	1/K
Heat Capacity at contact pressure	132	J/(kg.K)
Density	19350	kg/m ³
Thermal Conductivity	174	W/(m.K)
Young's modulus	4.11E+11	Pa
Poisson's ratio	0.28	1

Fig.7 represent the initial model drawing using COMSOL Software. Detail dimensional of the MEMS moisture sensor model is illustrated in Fig. 8.

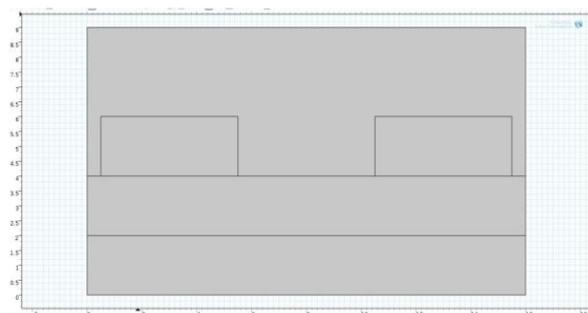


Fig. 7: Model drawing in the COMSOL Multiphysics Software

Fig. 8 shows the MEMS moisture sensor model that was extruded with 5µm length. A thin silicon dioxide was deposited in order to give a capacitive properties of the structure while the silicon at the bottom layer was used as the substrate in the structure. After the material selection for modelling the structure was done, the boundary condition was set accordingly by selecting the appropriate physics setup. The physics setup in the COMSOL Multiphysics software that was employed for this study were "Electro-mechanics" and "Heat Transfer in Fluid". The electro-mechanics physic is used for modelling the boundary condition for the terminal and ground electrodes surface. The voltage of the terminal electrode was set at 1Volt. The modelling of the boundary condition of the heat transfer in fluid physic is representing the surrounding air domain condition, where the humidity and the temperature were set accordingly.

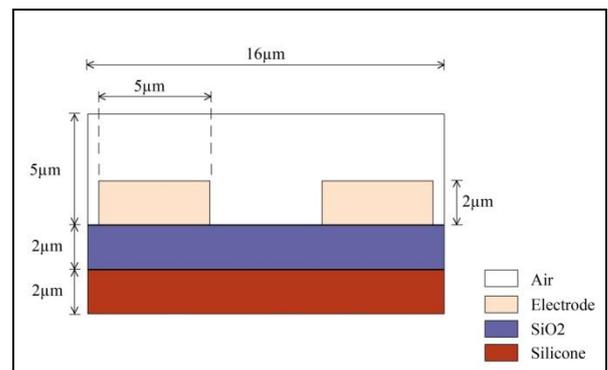


Fig. 8: Cross section dimension of the model in COMSOL Multiphysics

3. Result and Discussion

The reference model is obtained from the validation model. The validation process was done by comparing the simulation results of the constructed MEMS moisture sensor via COMSOL Multiphysics software against the actual experimental results in [5]. The percentage of error between the simulation and experimental results should be less than 10% [6, 7]. Noriah Yusoff et al and Rosli Darmawan et al asserted that if the simulation result of the reference model is less than 10% as compared against the actual result then the model can be validated and accepted as a reference model [6, 7]. Table 2 shows the percentage of error between the capacitance value of the experimental study and capacitance value of the simulation model. The percentage of errors were calculated according to the various temperature and RH setting. The overall percentage of errors obtained were less than 10%. Therefore, the constructed MEMS moisture sensor simulation is validated and can be accepted as a reference model. The simulation model was validated against the experimental model with 4.39% error; less than 10% as suggested by [6].

Table2: Percentage of error between the simulation and experimental study of the capacitance value; Reference Model.

Temp. (°C)	Relative Humidity (RH) (%)	Capacitance in Previous Study (pF)	Capacitance from the simulation (pF)	Error (%)	Sensitivity, S pF/(%RH)
25	50.00	190.85	186.00	2.54%	3.70
	70.00	280.42	260.00	7.28%	
	90.00	320.43	334.00	4.23%	
35	50.00	192.03	192.00	0.02%	3.83
	70.00	280.25	269.00	4.01%	
	90.00	320.53	345.00	7.63%	
45	50.00	191.84	198.00	3.21%	3.98
	70.00	279.89	277.00	1.03%	
	90.00	325.77	357.00	9.59%	
Average sensitivity					3.84

From Table 2, the sensitivity of the sensor was defined as the change in output of the sensor per unit change [8]. Equation (1) shows the equation that been used to calculate the sensitivity of the sensor [9].

$$\text{Sensitivity, } S = \frac{C_{H_2} - C_{H_1}}{H_2 - H_1} \tag{1}$$

Where,

C_H = Capacitance Value at the humidity of H
 H = Humidity

As an example; from Table 2 in green shading at the RH range of H_2 and H_1 is in between RH90 and RH50, the range value of capacitance is in between 186 and 334. The average sensitivity of the reference model 25 °C temperature, different humidity was 3.83 pF/ (% of humidity). Correspondingly, the average sensitivity of

the sensor in the group of the same humidity with different temperature setting was 0.87 pF/°C. The validated model was then used to further explore the sensor performance and eventually the optimize design parameters were established. In this study two main parameters were investigated, the width of the electrode and the gap between electrodes; A and B respectively (refer to Fig.9). Then the simulation results based on the output capacitance value were evaluated accordingly. Fig. 9 is the constructed according to the reference model except for electrode's width and gap between the electrodes are labelled as A and B respectively.

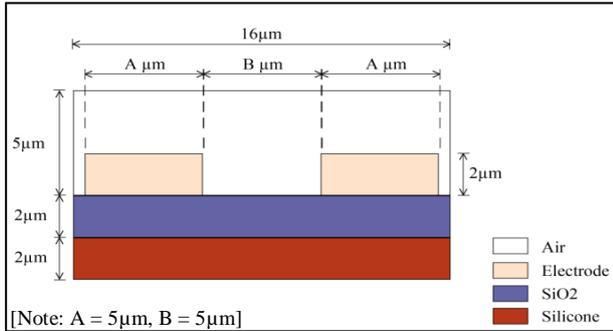


Fig. 9: Dimension of the improvised MEMS moisture sensor model.

The first modification was made by reducing the gap between electrodes to 3µm (B=3µm) while maintaining the electrode width, A at 5µm. Table B displays the simulation results of the first modification done.

Table 3: Capacitance value when the width of the electrode (A) is 3µm

Temp (°C)	Relative Humidity (%)	Capacitance Value (pF)		Sensitivity, S (pF/%RH)
		Reference Model (pF)	Improved Model (Simulation result) (pF)	
25	50	186.00	200.00	4.00
	70	260.00	280.00	
	90	334.00	360.00	
35	50	192.00	207.00	4.13
	70	269.00	289.00	
	90	345.00	372.00	
45	50	198.00	213.00	4.28
	70	277.00	299.00	
	90	357.00	384.00	
Average Sensitivity				4.14

Table 3 exhibits the capacitance value of the improvised design with 3µm width of every IDE fingers. The sensitivity calculated and presented in Table 3. The average sensitive is of the improvised Model 1 is 4.14 pF/%RH and 0.93 pF/°C.

The second modification was done by changing the electrode width, A to 6µm and maintaining the gap, B at 5µm. The result of the second modification is presented in Table 4. The average sensitive of the improvised Model 2 is 4.15 pF/%RH and 0.93 pF/°C.

Table 4: Capacitance value when the distance between the electrodes (B) is 6µm

Temp (°C)	Relative Humidity (%)	Capacitance Value (pF)		Sensitivity, S (pF/%RH)
		Reference Model (pF)	Improved Model (Simulation result) (pF)	
25	50	186.00	200	4.03
	70	260.00	281	
	90	334.00	361	
35	50	192.00	207	4.15
	70	269.00	290	
	90	345.00	373	
45	50	198.00	214	4.28
	70	277.00	299	
	90	357.00	385	
Average Sensitivity				4.15

The third modification of the model was made by changing the electrode width A to 6µm while the gap B is maintained at 5µm; similar to the reference model. The result of the third modification is presented in Table 5. The average sensor sensitivity of the improvised Model 3 is 4.15 pF/%RH and 0.95 pF/°C.

Table 5: Capacitance value when the width of the electrode (A) is 6µm

Temp (°C)	Relative Humidity (%)	Capacitance Value (pF)		Sensitivity, S (pF/%RH)
		Reference Model (pF)	Improved Model (Simulation result) (pF)	
25	50	186.00	201	4.03
	70	260.00	282	
	90	334.00	362	
35	50	192.00	208	4.15
	70	269.00	291	
	90	345.00	374	
45	50	198.00	215	4.28
	70	277.00	301	
	90	357.00	386	
Average Sensitivity				4.15

The fourth modification was made by reducing the gap B to 3µm while the length A is maintained at 5µm. The result of the fourth modification is presented in Table 6. The average sensor sensitivity of the improvised Model 4 is 6.12 pF/%RH and 1.38 pF/°C.

Table 6: Capacitance value when the distance between the electrodes is 3µm

Temp (°C)	Relative Humidity (%)	Capacitance Value (pF)		Sensitivity, S (pF/%RH)
		Reference Model (pF)	Improved Model (Simulation result) (pF)	
25	50	186.00	295	5.93
	70	260.00	414	
	90	334.00	532	
35	50	192.00	305	6.13
	70	269.00	428	
	90	345.00	550	
45	50	198.00	315	6.33
	70	277.00	441	
	90	357.00	568	
Average Sensitivity				6.13

Fig. 10 compares the capacitance values of the simulation results in Table 3; Model 1, Table 4; Model 2, Table 5; Model 3 and Table 6; Model 4 at 25°C against the reference model (Table 2). The graph trends show that the line capacitance value from Table 6; Model 4 achieved the highest capacitance value compared to the rest. Table 6 is the result from the improvised Model 4 where the gap between the electrodes was reduced from 5µm to 3µm. When the gap between the electrodes is smaller, the capacitance value of the sensor is higher which because of the stronger electrical field between the electrodes. Results from Table 5 (Model 3) and Table 3 (Model 1), indicate the capacitance values that were generated from the improvised Model 3 and Model 1 are at par to each other; the width electrode (A) of 6µm and 3µm. respectively This finding point out that changes in between the electrode gap is giving more impact rather than the electrode width.

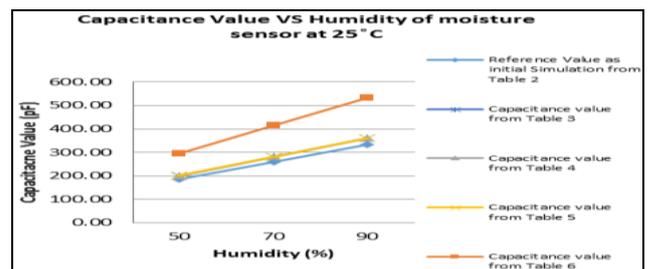


Fig. 10: Graph from the result of reference model and improvised model at 25°C.

4. Conclusion

The understudied moisture sensor was successfully simulated and validated using the COMSOL Multiphysics software. The simulation result shows that the sensor device is more sensitive to humidity rather than the temperature. This attribute is in agreement with the main objective of the moisture sensor development; highly sensitive to the moisture presence. The key findings from this research are, by reducing the electrodes' gap closer to each other, it helps to increase the sensitivity of the sensor. Also, changes in the electrode geometrical size does not give significant impact to the capacitance reading. These findings suggest that reducing the gaps in between the electrodes with the appropriate electrode width are the promising solutions in optimizing the sensor performance.

Acknowledgement

We would like to thank Research Management Institute of Universiti Teknologi MARA (UiTM) for fully funding this research project under the BESTARI Research Grant Scheme (600—IRMI/MyRA 5/3/BESTARI (012/2017)).

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